



ENERGY EFFICIENCY OPTIMISATION

EFFICIENCY OPTIMISATION

Genova, September 2013

Martial CLAUDEPIERRE

Business Development Manager
Environmental Services

Green Shipping Summit

Move Forward with Confidence



BUREAU
VERITAS

Content

- ▶ Who we are
- ▶ How to improve the energy efficiency of ships ?
- ▶ Energy efficiency tools and solutions
- ▶ Case studies



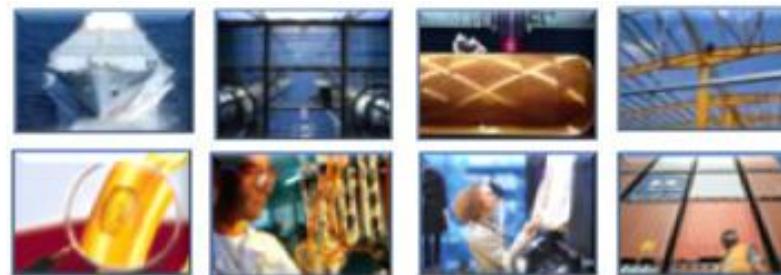
Bureau Veritas : what we do

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OUR SERVICES

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EMISSIONS REGULATION

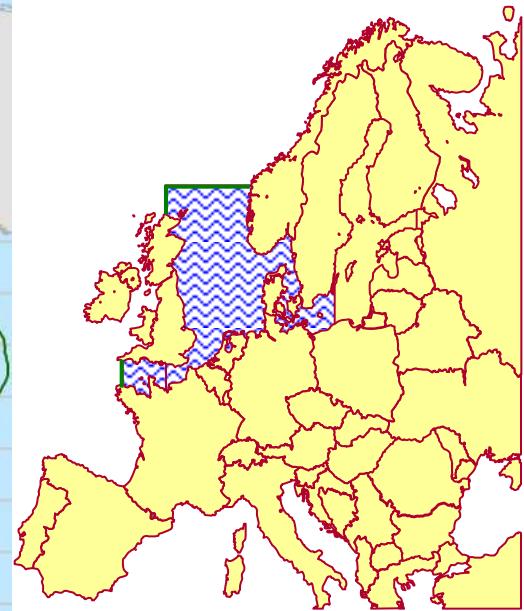
UPDATES

Emission Control Areas (ECA)

► An Emission Control Area :

- NOx, SOx and particulate matter, or
- all three types of emissions.

► Existing ECA and SECA are today:



Baltic Sea (SOx)	26 Sept 1997	19 May 2005	19 May 2006
North Sea (SOx)	22 Jul 2005	22 Nov 2006	22 Nov 2007
North American (SOx, and NOx and PM)	26 Mar 2010	1 Aug 2011	1 Aug 2012
United States			
Caribbean Sea ECA (SOx, NOx and PM)	26 Jul 2011	1 Jan 2013	1 Jan 2014

International Regulations for SOx emissions

Regulations	Sulphur Content (in mass)				
	2010	2012	2015	2020 or 2025	
IMO – Global (except for passenger ships)	4.5%	3.5%			
IMO – ECA – SECA (EU aligned with IMO)	1.5%	1.0% (since 01.07.2010)	0.1%		
EU ports	0.1%				
California (< 24 nm)	1.5% (MGO) 0.5% (MDO)	0.1%			

- With effect from 18 December, 2012, the EC Sulphur Directive 1999/32/EC is amended by Directive 2012/33/EU in order to align the EC regulations on sulphur content of marine fuels with the IMO regulations.
- The EC regulations **are aligned** with the revised Annex VI to MARPOL, both inside and outside EU SOx Emission Control Areas (SECA). The 0.50% limit outside EU SECAs will apply in EC waters from 1 January, 2020, **regardless of the outcome** of the IMO fuel availability review, which is due by 2018.
- Emission abatement methods (e.g. exhaust gas cleaning systems) **are permitted** for ships of all flags in EC waters as long as they **continuously achieve** reductions of SOx emissions which are **at least equivalent** to using compliant marine fuels.



EEDI and Design innovations

The EEDI of ships is to be calculated according to IMO guidelines:

- Original document : MEPC Circ.1/681
- Calculation guidelines adopted at MEPC 63: Resolution MEPC 213(63)
- Formula:

$$\left(\prod_{j=1}^M f_j \right) \left(\sum_{i=1}^{nME} P_{ME(i)} \cdot CF_{ME(i)} \cdot SFC_{ME(i)} \right) + \cancel{P_{AE} \cdot C_{FAE} \cdot SFC_{AE} * \cancel{\left(\prod_{j=1}^M f_j \cdot \sum_{i=1}^{nPFI} P_{PTI(i)} - \sum_{i=1}^{neff} f_{eff(i)} \cdot P_{AEeff(i)} \right) C_{FAE} \cdot SFC_{AE}}} - \left(\sum_{i=1}^{neff} f_{eff(i)} \cdot P_{eff(i)} \cdot C_{FME} \cdot SFC_{ME} ** \right)$$

$f_i \cdot f_c \cdot Capacity \cdot f_w \cdot V_{ref}$

Ship's work in normal operating condition

Impact of Main Engines

Impact of auxiliary power demand

Impact of PTI reduced by electrical innovations

Reduction of impact due to mechanical innovations

f	Correction factors
CF	CO_2 emission coefficient
SFC	Specific fuel consumption
"AE"	Subscripts for auxiliary engines
"ME"	Subscripts for main engine(s)

Target Years & Reduction Rates

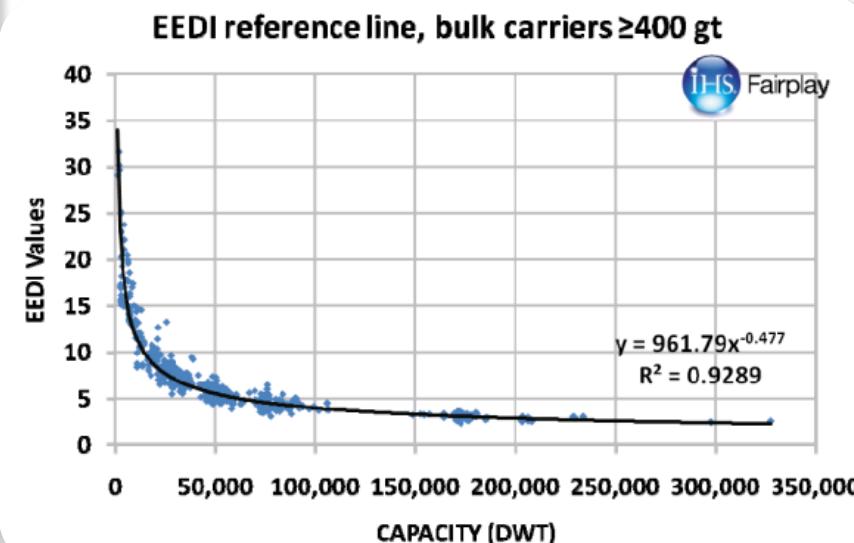
Draft regulatory text for mandatory EEDI requirements: target years & reduction rates

Ship Type	Size	Phase 0 1 Jan 2013 – 31 Dec 2014	Phase 1 1 Jan 2015 – 31 Dec 2019	Phase 2 1 Jan 2020 – 31 Dec 2024	Phase 3 1 Jan 2025 onwards
Bulk Carrier	20,000 DWT and above	0	10	20	30
	10,000 – 20,000 DWT	n/a	0-10*	0-20*	0-30*
Gas tanker	10,000 DWT and above	0	10	20	30
	2,000 – 10,000 DWT	n/a	0-10*	0-20*	0-30*
Tanker	20,000 DWT and above	0	10	20	30
	4,000 – 20,000 DWT	n/a	0-10*	0-20*	0-30*
Container ship	15,000 DWT and above	0	10	20	30
	10,000 – 15,000 DWT	n/a	0-10*	0-20*	0-30*
General Cargo ships	15,000 DWT and above	0	10	15	30
	3,000 – 15,000 DWT	n/a	0-10*	0-15*	0-30*
Refrigerated cargo carrier	5,000 DWT and above	0	10	15	30
	3,000 – 5,000 DWT	n/a	0-10*	0-15*	0-30*
Combination carrier	20,000 DWT and above	0	10	20	30
	4,000 – 20,000 DWT	n/a	0-10*	0-20*	0-30*

* Factor to be linearly interpolated between two values dependent upon vessel size (the lower value of reduction factor is to be applied to the smaller ship size).

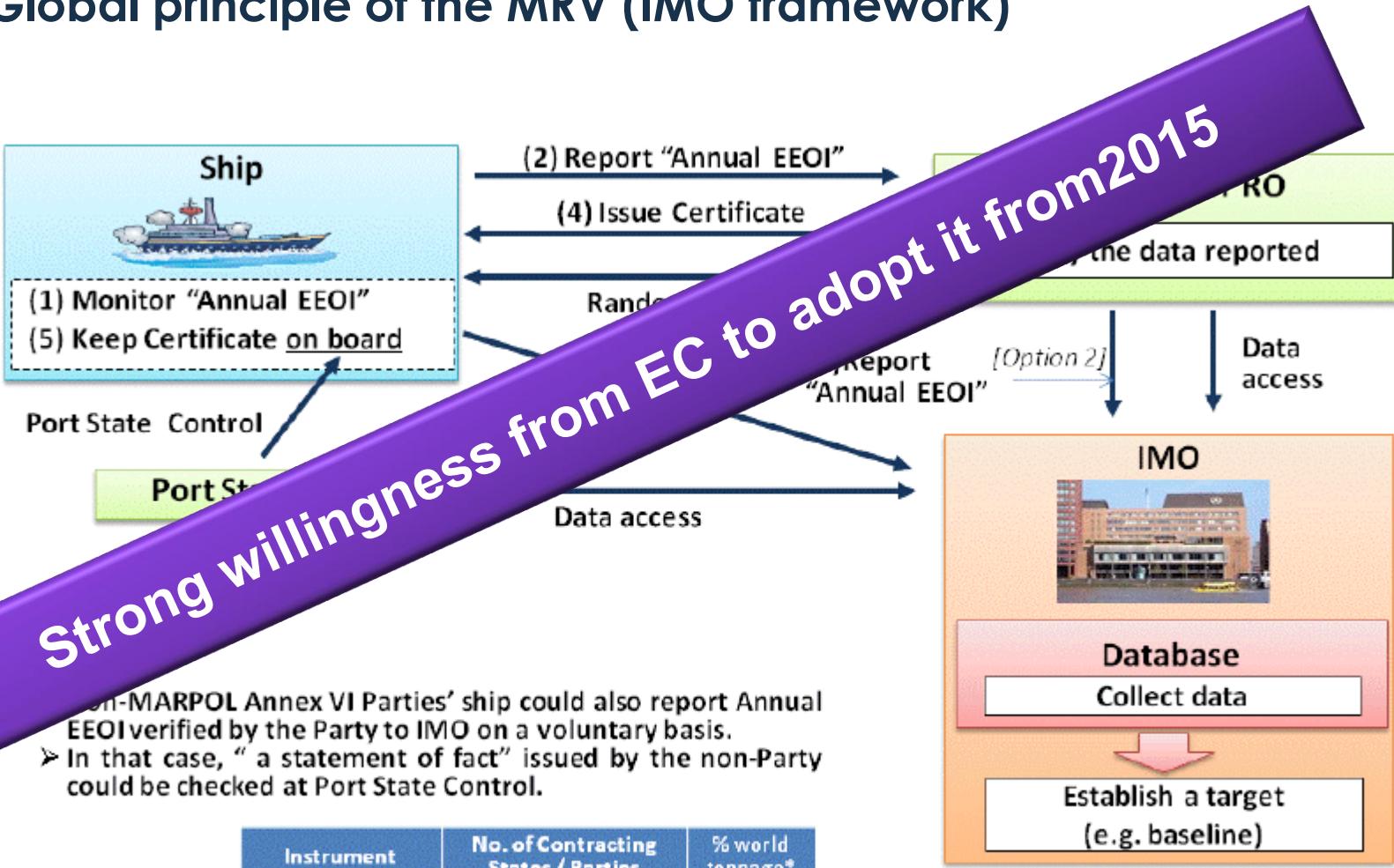
$$EEDI_{attained} \leq EEDI_{required}$$

$$EEDI_{required} = \left(1 - \frac{X}{100}\right) \times \text{Baseline value}$$



Monitoring Review and Monitoring MRV

► Global principle of the MRV (IMO framework)



* Source: IHS-Fairplay - World Fleet Statistics 31 December 2011



HOW TO IMPROVE ENERGY EFFICIENCY ?

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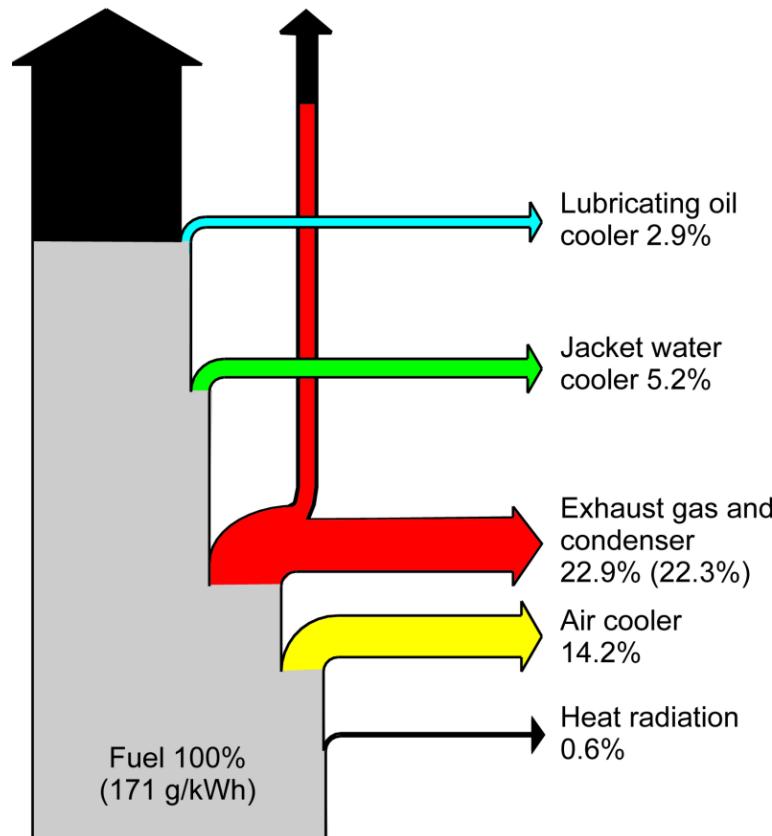
Where energy & money go ?

Total power output 54.2% (54.8%)

Shaft power output 49.3%

El. power production of TES 4.9% (5.5%)

Gain = 9.9% (11.2%)

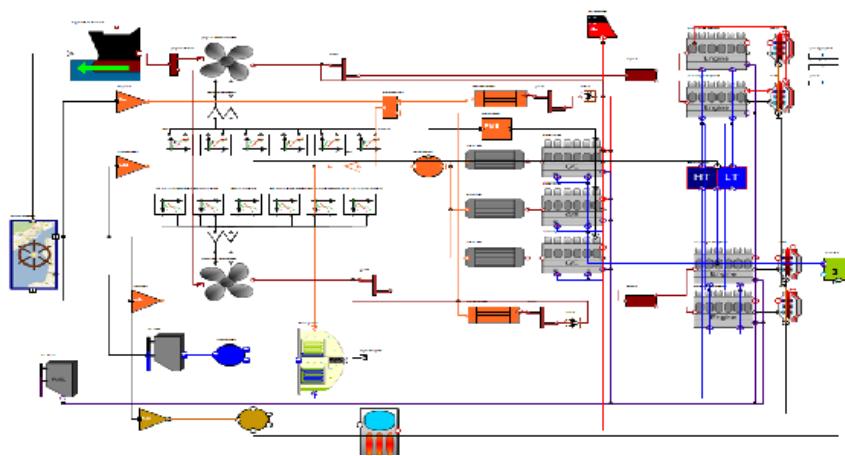


Understanding the energy balance is the key for deciding where efforts shall be put for recovering of energy losses and optimisation of the efficiency of your OSV.

The energy balance is to be calculated at design stage, estimated with simulating tool such as SEECAT, and/or measured onboard through initial **energy audit** and **onboard instrumentation** systems.

Different propulsion configurations & potential savings

- ▶ Different combinations can be envisaged between Electric propulsion and Mechanical propulsion with CPP
- ▶ CAPEX is higher for Electric drive, OPEX is lower
- ▶ Savings are possible in the low loads. At low pitch, losses are high due to poor optimisation of the CPP at that point,
- ▶ But an holistic approach is recommended to assess consequences on energy recovery systems for example
- ▶ I will introduce our third party verification tool SEECAT further down



Hull & propeller fouling management

Maintenance measures implemented during the scheduled maintenance periods are « low hanging fruits » for improving the energy efficiency without impacting on the design of the ship and her components.

Fouling depends on localisation, season, and operational profile (time spent anchored on tropical sea).

There are big variation in performance between coating solutions on the market.

It is challenging to measure and assess the loss of speed due to growing.

However some models can be elaborated.

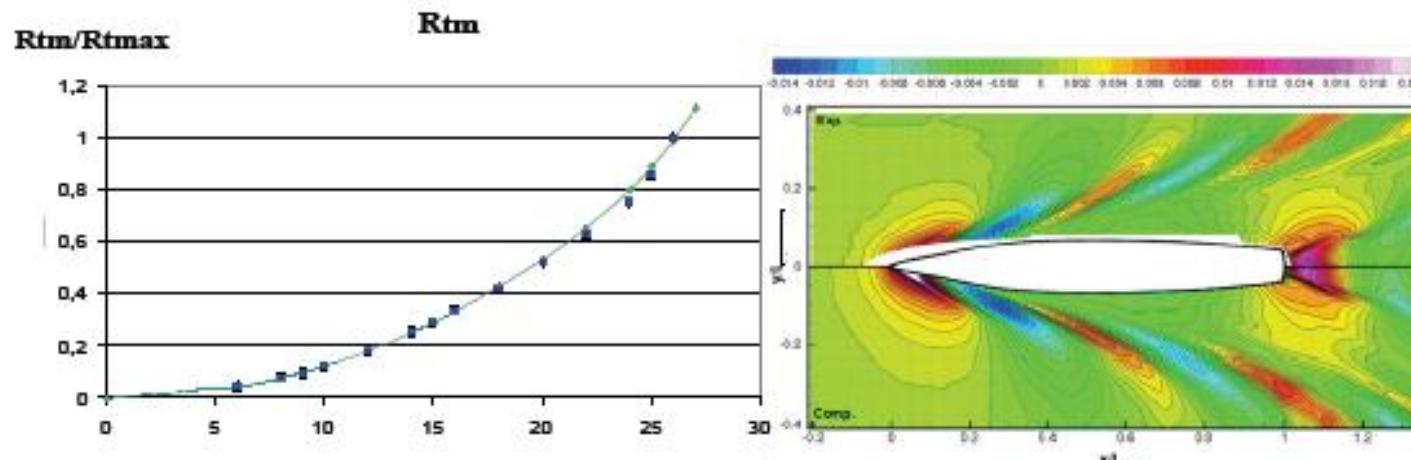
Coating application at a right schedule will improve the efficiency. We will learn from an on-going case study exposed further

But frequent cleanings could deteriorate the coating requiring pre-mature re-coating or leading to decreased vessel performance.

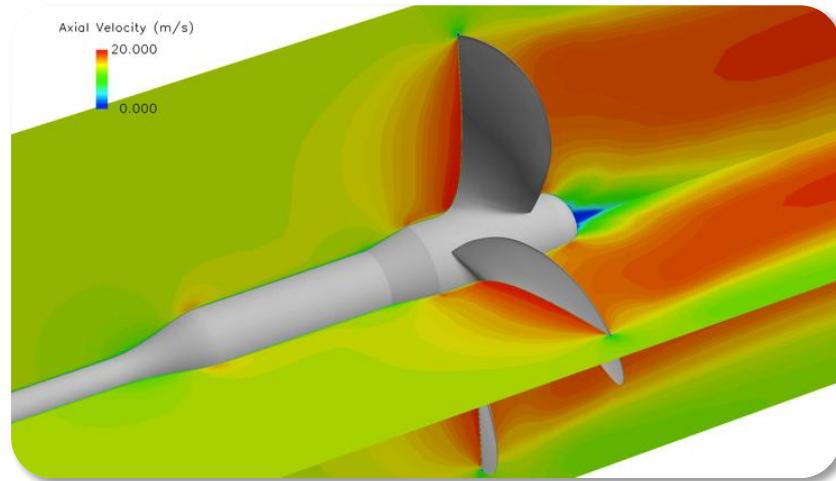


Hull form optimisation by CFD calculation

- ▶ Hull form optimization should be based on a selected combination of drafts, trims and speeds.
- ▶ **Hull form optimisation requires : Adapted Numerical solvers**
- ▶ **Navier-Stokes with free surface flow solvers** are more accurate, very close to model test results but CPU time consuming, and license cost expensive
- ▶ Complex automatic meshing for 3D volume meshes
- ▶ **Exemple : Optimisation on 10 operational conditions, 50 hull forms**
- ▶ • Total of 500 CFD computations
- ▶ • 1 CFD calculation needs 1 license for 32 cores, 10 h on 32 cores
- ▶ • Total of $10 \times 32 \times 500 = 160\,000$ CPU hours



■ Description: unsteady CFD simulations of a rotating propeller

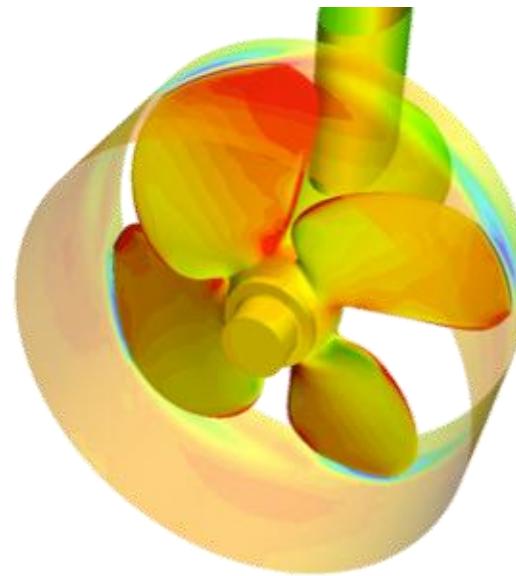


■ Outputs of the simulations:

- **K_t , K_q and efficiency of the propeller in open water**
- **Estimation of cavitation onset risks**

■ Example of applications:

- **Evaluation of propeller performances**
- **Evaluation Energy Saving Devices close to propeller**



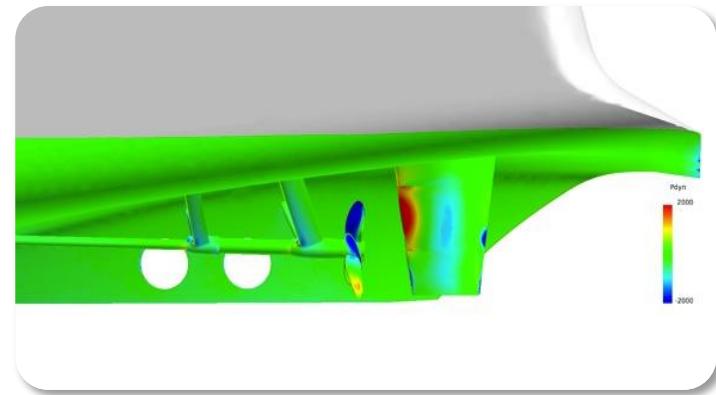
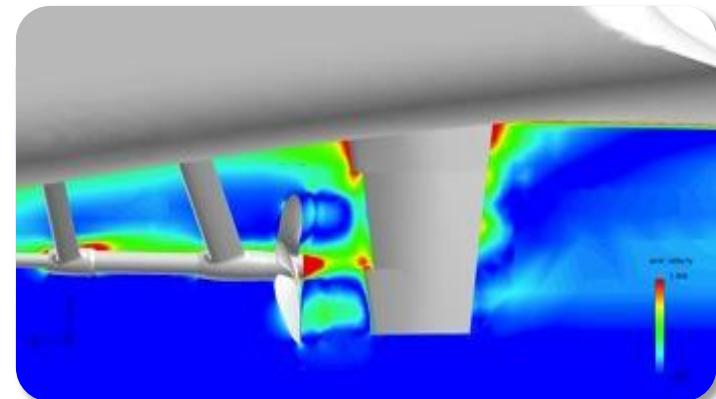
■ Description: unsteady CFD simulations of hull and appendages, including rotating propeller

■ Outputs of the simulations:

- Propulsive performances of the ship
- Evaluation of hull/ propeller/ appendages interactions
- Cavitation onset risk, pressure pulses ...

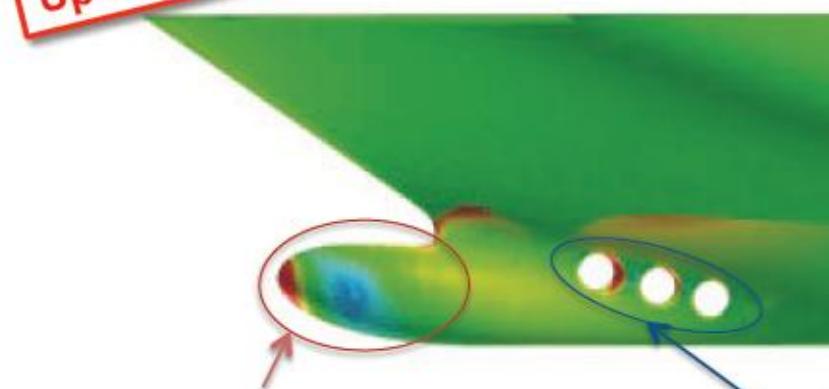
■ Example of applications:

- Hull power optimisation
- Appendages alignment (twisted rudder and shaft brackets ...)
- Evaluation of several propellers performances



VeriSTAR Energy Efficiency – Hull Form Optimisation

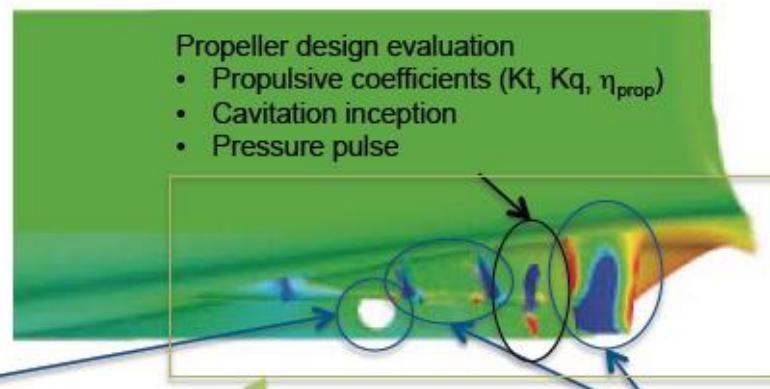
General hull shape parametric optimisation in resistance (curve section area, main hydrostatics)



Bulbous bow shape parametric optimisation. Total drag and wave field reduction.

Bow or stern thrusters shape optimisation.

- Orientation of level on flow
- Evaluation of Energy Saving devices



Stern, wedges, ducktail shape optimisation in presence of propeller ((1-t), (1-w), η_{hull})



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HydrOcean

Expertise in Marine Hydrodynamics

LNG as fuel

- ▶ NOx emissions reduced by more than 80% (for lean burn engines). ...
- ▶ SOx emissions eliminated (no sulphur in LNG).
- ▶ Particulate matters are close to zero.
- ▶ CO2 emissions are reduced by approx. 20% (unburned methane if any should be taken into account as its global warming potential is high).



LNG bunkering solutions

► Bunkering arrangements

- For small capacities, non-fixed tanks located onboard the can be arranged, such as containerized tanks or truck trolley tanks.
- Bunkering from land based LNG storage facility is also a solution in some circumstances
- For larger capacities, bunkering from a dedicated bunker ship will be used. Alternatively, bunkering from LNG terminals is also considered subject to relevant agreements **from flag and port authorities** and safety analysis.



Ship-to-ship LNG transfer



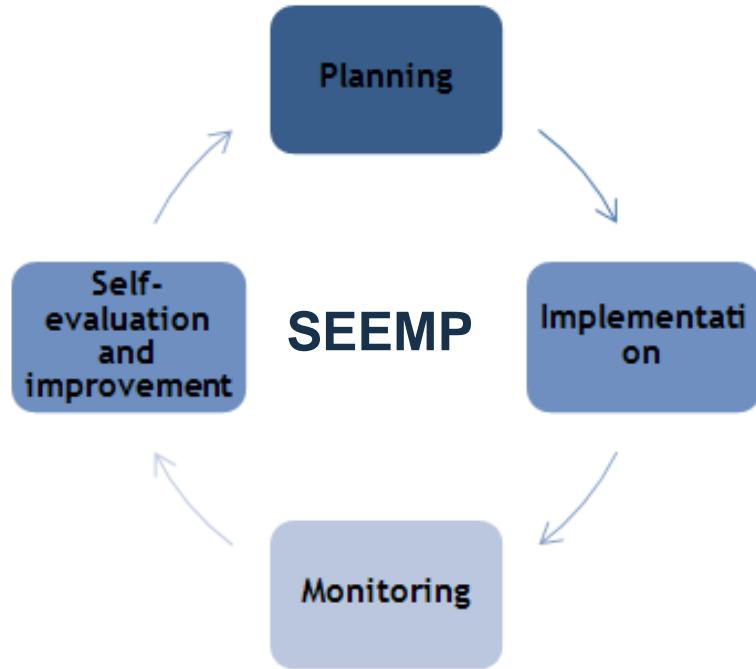
system type-approved by BV



**HOLISTIC APPROACH FOR
ENERGY EFFICIENCY IMPROVEMENT**

SEECAT TOOL

Energy Saving Measures – How to focus on the right ones?



Letter	Order of magnitude
A	Saving > 20%
B	10 < Saving < 20%
C	5 < Saving < 10%
D	2,5 < Saving < 5%
E	1 < Saving < 2,5%
F	Saving < 1%
Energy Efficiency improvement measures	
Weather routing	D
Just in time arrival	D
Speed optimization	D
Super Slow Steaming	A
Optimum trim	D
Optimum ballast condition	D
Hull coating cleaning	C
Propeller cleaning and polishing	C+
Engine auto-tuning	D
Main engine derating	E
Main engine variable turbo area	E
Use of alternative fuels	B
Waste Heat Recovery System	B-C

► The challenge is to know how to optimally combine several measures to obtain a fuel efficient and environmentally friendly ship.

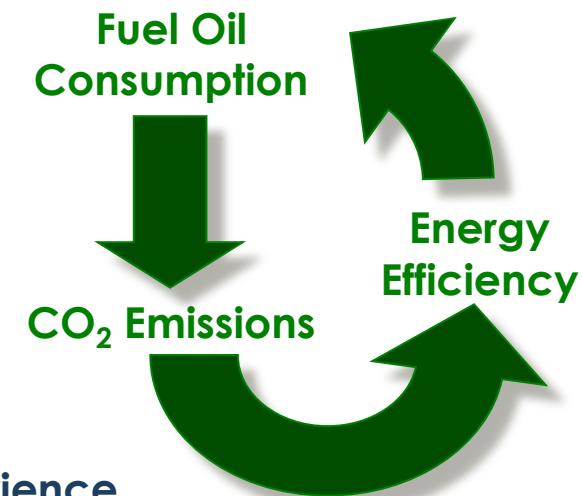
Global Approach for Improving Energy Efficiency

It is necessary to adopt an **holistic approach** when improving a ship in operation

Only a specific **energy transfer** equations calculation **tool** can provide a third party **global gain prediction at ship scale**

■ Fuel oil consumption for can be reduced by:

- Operational measure
- Improved maintenance measures
- Retrofitting Energy Saving Devices on hull, propeller, machinery



■ Add all the potential gain (generally communicated by suppliers) and you end up with 50% - did you experience such improvement? Of course not !!

■ There are so many interactions, for example reducing speed will impact on WHB efficiency, meaning oil fired boilers to be run...

■ We decided to adopt a fair and global approach

SEECAT: Ship Energy Efficiency Calculation and Analysis Tool

Purpose of the SEECAT tool:

- Create the energy model of a ship
- Establish the energy balance and calculate the energy efficiency of the ship
- Calculate the fuel consumption and emissions (NOx, SOx, CO2)

Energy Flow Modeling – Basic Idea

The ship's power needs should be fulfilled by the power producing units



Example of Results

Ship modeling

Fuel consumption

CO2 emissions

Speed profile

Library

Model1 (ship_v5.3.ism)

Ship modeling

Fuel consumption

CO2 emissions

Speed profile

SignalBlocks

Model Explorer

Output

Simulation finished successfully! (ship_v5.3.ism)

Simulation Time: 590400.0000000000 s

SimulationX Professional Edition - ship_v5.3.ism

File Edit View Insert Elements Simulation Analysis Export Extras Window Help

Transient

Libraries

Three phase alternator

Combustion engine

Engine model based on a brake specific fuel consumption curve

ExhaustGas

emission box

Waste heat recovery boiler

Fuel

Fuel tanks

Fuel switch with connector as table

NewModel1

Shared library for common models

ship's hull, resistance, propeller

Speed setting

output of R/V²

use of R/V²

use of R/V²

Ship resistance model (contains HoltropMennem and ShipHull model)

Speed setting

Mechanics

Operational profile definition

Global A33 ship data - RENAME IN : 'shipData'

FWProfile

Electricity Consumption

Maximum absorbed power by different electricity consumers

Global ship data

Power management system

Electrical switchboard

Power Management System module

producers and consumers

Steam consumption Profil

Steam Conso

SteamSource

Boiler

Exchanger Steam Evaporator

NewPackage1

FWEvaporator

EMCone

Comment: Signal Blocks

Ident: SignalBlocks

Version: 3.4

File: C:\Program Files\ITI-Software\SimulationX\3.4\Libraries\cosimulation.cat

Output

Simulation finished successfully! (ship_v5.3.ism)

Model Explorer

Comment Name Current Value Unit

Gravity Acceleration gravity 9.80665 m/s²

Gravity Acceleration (3D) gravit... {0,0,-gravity} m/s²

Ready



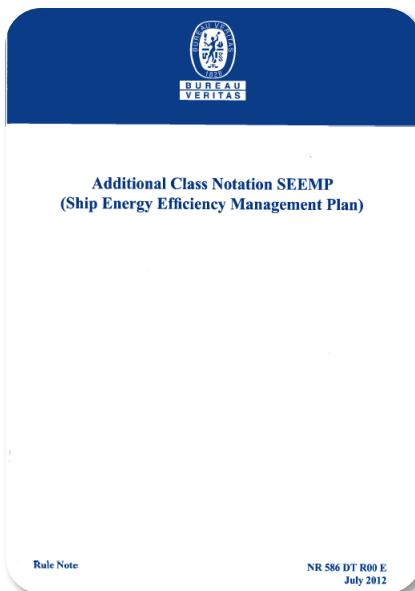
BV Ship Energy Efficient (SEE) Notation

BV Additional Notation SEE, SEE-OP and SEE-MON

The additional class notation SEE is defined in BV NR 586 “SEE Additional Class Notation” and deals with the voluntary approval and periodical inspection of the SEEMP.

The (revised) notation SEE includes now:

- Two levels: review of initial plan (SEE) and review of plan and inspections in service (SEE-OP)
- Introduction of SEE-MON for ships fitted with onboard measuring equipment (FO flowmeters, delivered power measurement, torque, draught, trim, navigation info)



Granting BV Additional Notation SEE - MON

Initial Energy Audit to set the Baseline

Validation of the SEEMP with the SEECAT Tool

Propulsion monitoring – Trim and draught monitoring
(water deep in some cases)

Machinery and Auxiliaries instrumentation



Principle : Calibration of the prediction tools with the real measurements (BV certified) onboard in order to get the accurate figures in further predicted consumption.



CASE STUDY 1

CH2E 210D11



Optimising Energy Efficiency in Operation

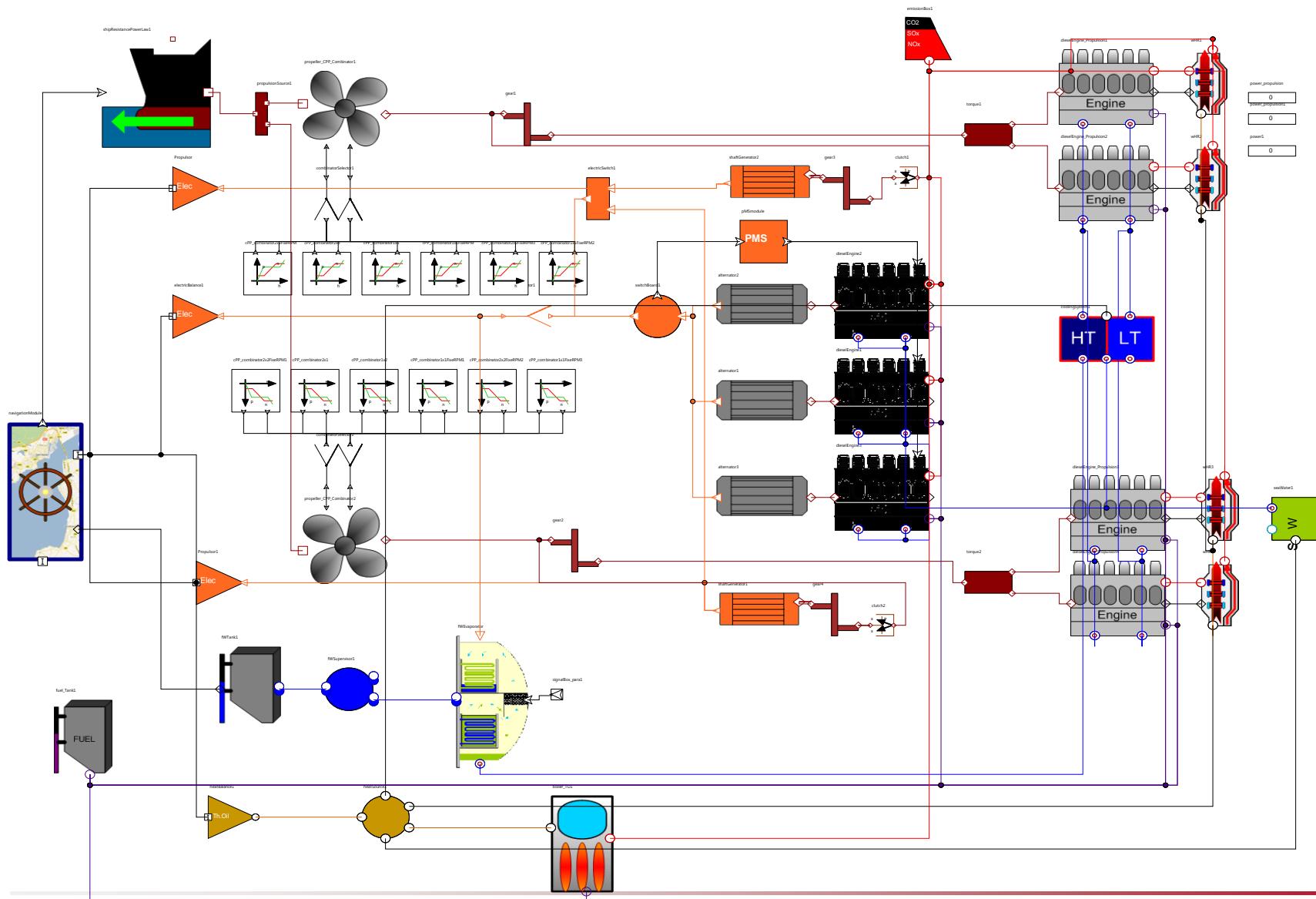
Guillaume Hagi – Brittany Ferries
Martial Claudepierre – Bureau Veritas

**The 35th Motorship
Propulsion & Emissions Conference**
24-25 April 2013
Copenhagen | Denmark





Energy model SEECAT of the Cap Finistère



SEECAT - Cap Finistère – fuel saving example

SEECAT- Application on Cap Finistère – In service optimisation

Configuration with clutched shaft alternators or unclutched (diesel generators started)

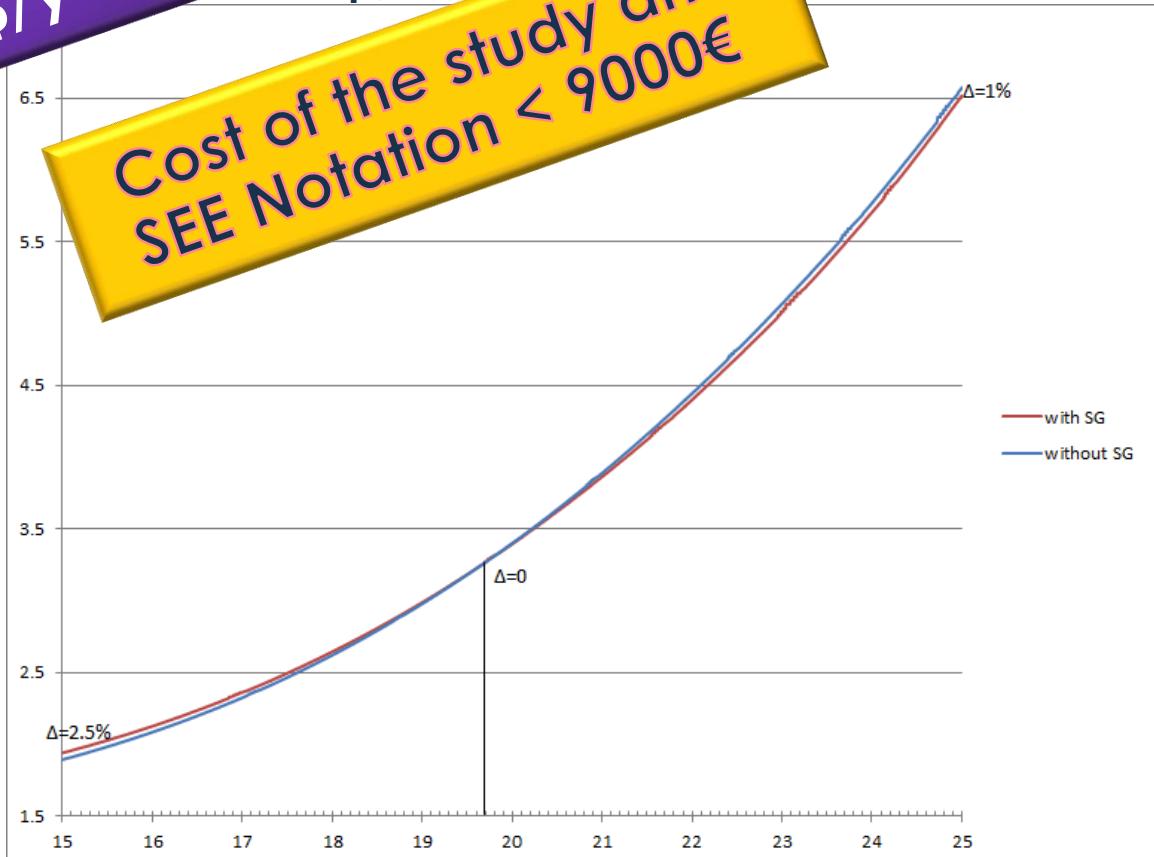
The power gain is calculated by the fuel consumption of the ship; Global approach according to the ship;

Optimum connections of the shaft alternators depending on rotation speed of the shaft lines and needed electrical power and efficiency of the diesel generators

The best operational and lower consumption are highlighted by SEECAT.

Potential saving of
180000 \$/year

Cost of the study and
SEE Notation < 9000€

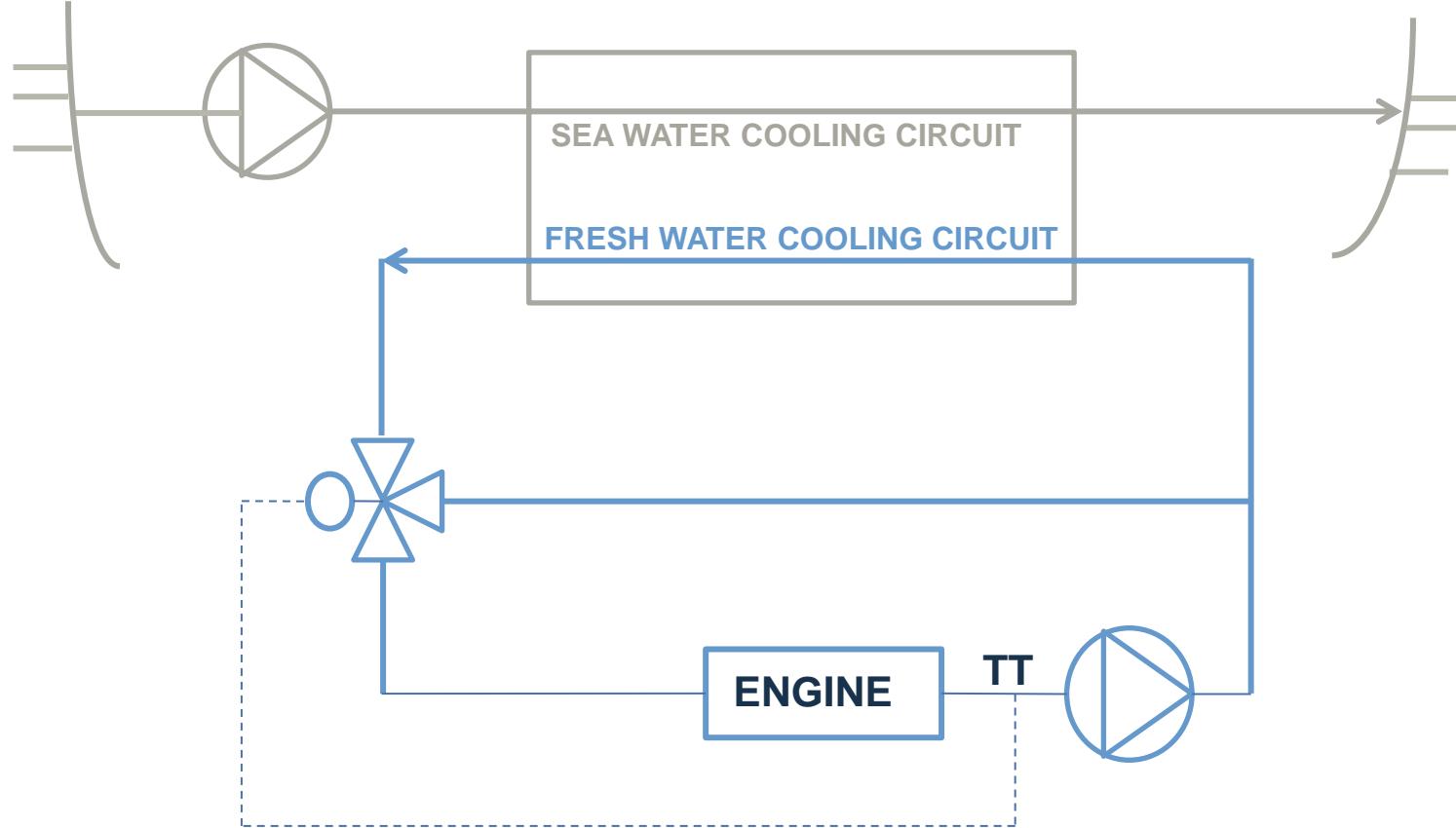




CASE STUDY 2

Case Study 2

Cooling of the main engine onboard a 8000 TEU

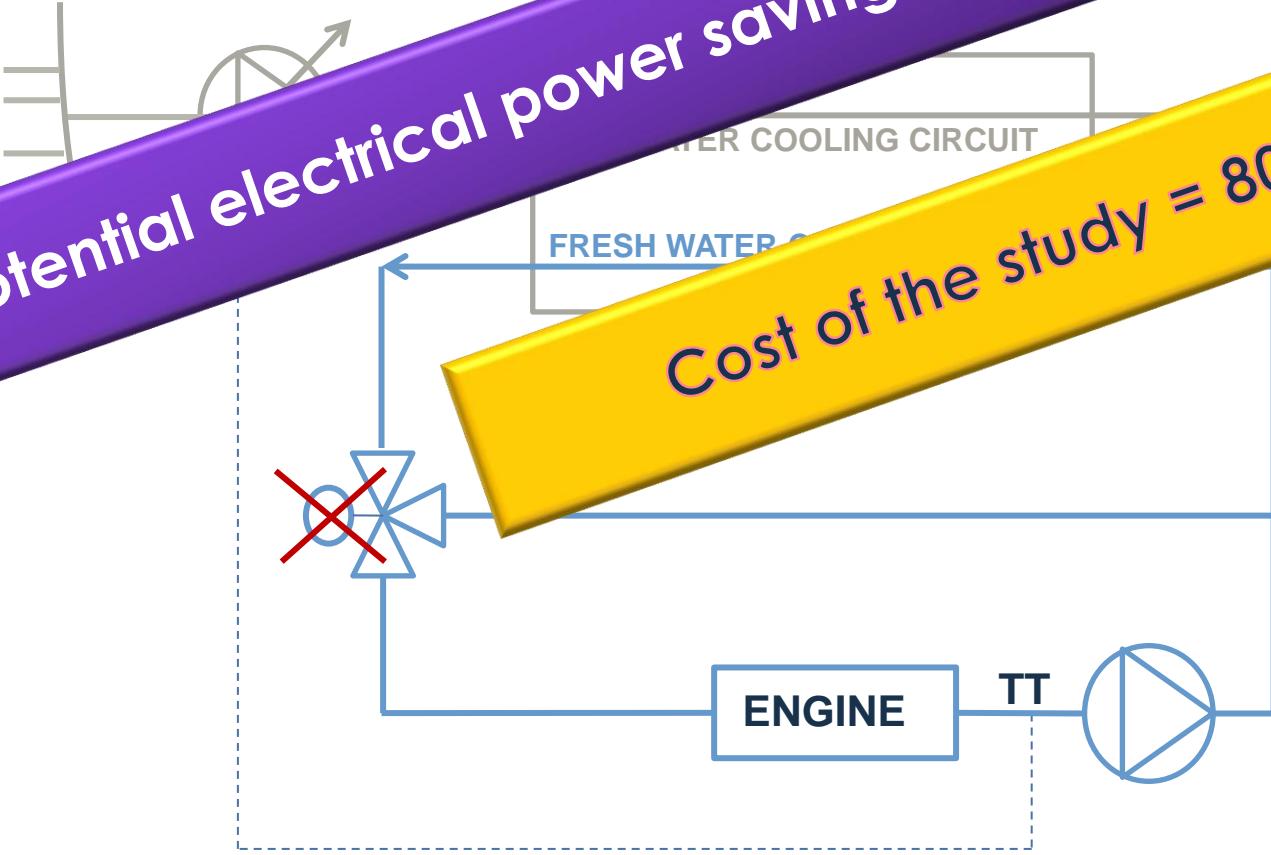


Optimisation of the cooling system with frequency variators



Potential electrical power saving of -70 % !

Cost of the study = 8000€



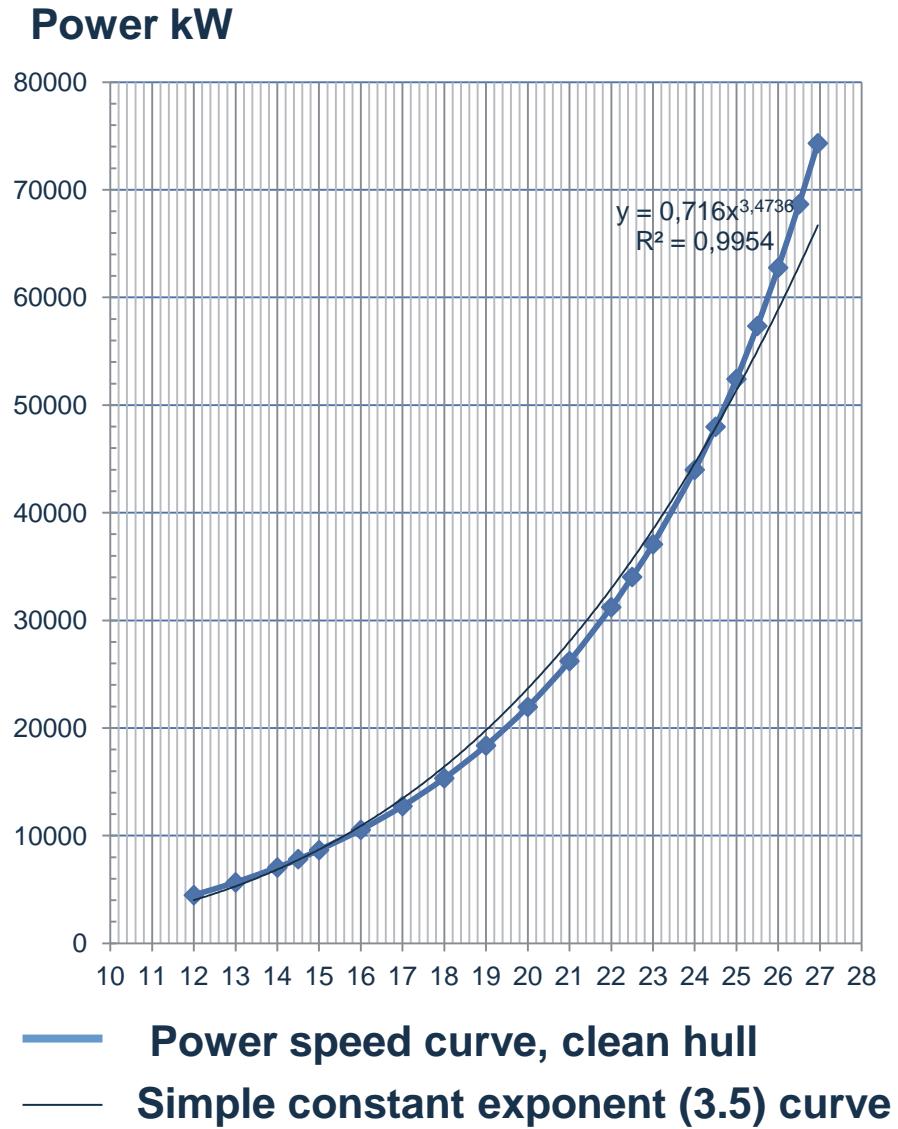


CASE STUDY 3

WIND ENERGY

Slow steaming and change of bulbous bow

- ▶ At low speed, the gain in necessary propulsion power can be considered as roughly a 3.5 power law curve.
 - In between 13 and 20 knots for container carriers
 - At 9 knots for a bulk carrier Capesize
- ▶ Thanks to the data collected during sea trials, towing tank tests or from CFD, BV will estimate using SEECAT the total fuel consumption at low load,
- ▶ Insight for changing bulbous bow will be given by additional CFD calculations from HydrOcean



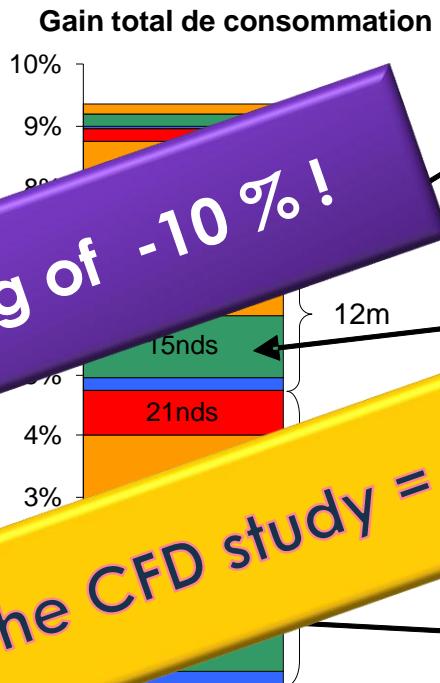
Slow steaming and change of bulbous bow

► Pre requested conditions:

- The original bulbous bow must have been optimised for high speed and loaded draft
- The slow steaming operations drastically different from (draft and speed)

- ▶ In the future, the potential for gains will be even greater on a large range of trial speeds.

- ▶ A large number of numerical calculations can be done for different parameters variations



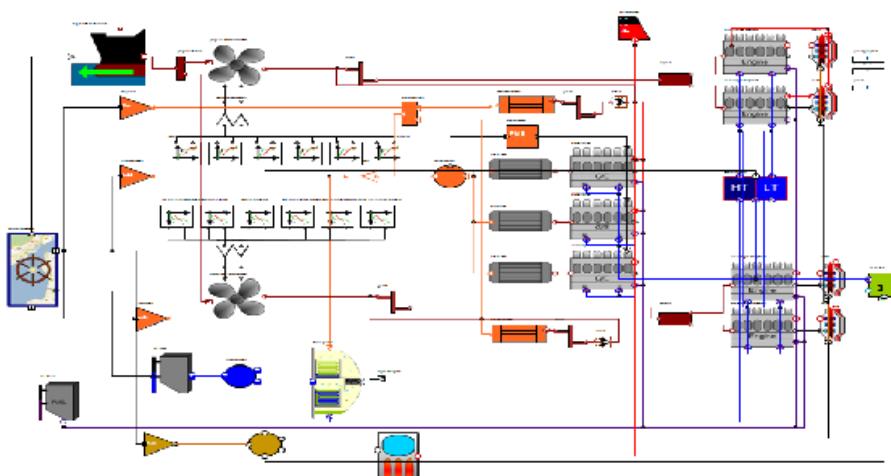


CASE STUDY 4

CH2E 210D1 +

Shuttle oil tanker in Brasil – effect of fouling on propulsive performance

- ▶ rpm, torque and thrust to be measured in both clean and dirty condition, then propeller and hull outputs are separated.
- ▶ The variation of the propulsive efficiency between both conditions of the propeller and hull to be calculated from the measurements.
- ▶ Predictions from the SEECAT model to be compared to the measurements, then the model to be calibrated for further predictions.



- ▶ As the ship displacement, and wind and sea conditions will not be exactly the same at both tests, the corresponding differences will be corrected.



LIST OF REFERENCES

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Any question?

